# **STEREO** *IMPACT*

FM2 STE-U Thermal Vacuum Test Report

IMPACT-STEU-FM2-TVac-Report.doc Version A – 2004-Aug-10

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# **Document Revision Record**

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# **Distribution List**

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# 1. Overview

#### 1.1. Introduction

STE-U is part of the STEREO IMPACT instrument suite. It resides at the sunny end of the IMPACT boom.

This document describes the results of the thermal vacuum testing performed on the FM2 STE-U unit. This testing was performed at U.C. Berkeley following the test procedure called out in reference 1. This report only covers the thermal cycling part of that test procedure. The FM1 thermal balance test results are discussed in a separate report.

#### 1.2. Applicable Documents

The following documents are closely interrelated with this specification. All documents can be found on the Berkeley STEREO/IMPACT FTP site unless otherwise indicated:

http://sprg.ssl.berkeley.edu/impact/dwc/

- 1. IMPACT STE-U TVAC TEST PLAN
- 2. APL Document APL 7381-9003 Rev A STEREO Environment Definition, Observatory and Instrument (on APL web site)
- 3. IMACT-IDPU-CPT



Fig 1. FM2 STE-U Unit

# 2. Test Setup

The "Jeffrey" thermal vacuum chamber at U.C. Berkeley was used. This is the chamber built for the IMPACT Boom thermal vacuum tests. It was used because it was the only chamber available at the time that could get cold enough.

STE-U thermal vacuum tests is complicated by the fact that the preamp portion has a significantly different temperature range from the detector portion. To accommodate this the preamp is hard-mounted to the baseplate and then covered with a thermal blanket (the same blanket that was used for STE-U thermal balance tests). The detector protrudes from this blanket so it can view the shrouds that were run cold. Radiation is insufficient to get the detector cold enough, so a heat strap was attached from the chamber cold plate to the detector. This allowed us to control the detector temperature more directly. Running the chamber with these gradients in it (rather than the usual isothermal thermal vac test) involved a learning curve. It was difficult to hit the correct temperature for both units. In some cases the temperature is somewhat beyond the required qualification level. Nothing was over-stressed during the test.

The IDPU was setup outside the chamber. This was the FM2 IDPU with the exception that the ETU LVPS was used (since the FM2 IDPU LVPS was not yet available). This plus GSE as described in the test procedure allowed us to test the instrument and monitor its internal temperatures.

In addition to chamber monitoring TCs (on the baseplate, cold plate, and shrouds), chamber TCs were attached to the instrument and GSE as called out in the test procedure. We were unable to get a TC to attach reliably to the STE detector without compromising the surface properties so TC11 was attached to the heat strap near the detector instead. The internal instrument TC was relied upon to measure the detector temperature. This temperature was found to be consistent with the heat strap temperature during soaks, less a few degrees lost across the joint between the heat strap and the detector.

# 3. Test History

#### 3.1. First Run

This test was first attempted starting on 2004-July-21. Following a long weekend 60 hour +40C bakeout / non op hot cycle, the instrument was transitioned to non-op cold. The first 3 and a half cycles proceeded uneventfully, but on cycle 4 hot the STE door status switch failed (see IMPACT PFR1013). The testing was discontinued and the unit was warmed up, removed and diagnosed. The door switch was adjusted and testing continued. Since the adjustment was minor, it was decided (together with the Project IM) to continue where we left off, at cycle 4, but starting with a door cycle test to verify reliability.

#### 3.2. Second Run

The unit was cooled down to cold soak and door cycling was attempted. Preliminary door motions looked fine, but automated door cycling caused the door to fail. The chamber was warmed up, and the instrument removed and diagnosed. It was determined that the automated door cycling left insufficient time for the actuator to cool off between actuations, which resulted in an actuator wire overheating and failing (see IMPACT PFR 1014). The door actuator wire was replaced. In addition, the flight software was modified to prevent attempts to actuate the door too close together. After discussions together with the Project IM it was determined that we would again continue from where we had left off, with the addition of some door cycles at the first cold soak to verify reliability.

### 3.3. Third Run

The unit was returned to the chamber and once again returned to cold soak cycle 4. The door was cycled 20 times (slowly, with 2 minutes between actuations) to verify door reliability, which went successfully. Cycling then continued uneventfully. In addition to the CPTs at each soak, a test of light sensitivity and bias voltage sensitivity were added to cold soak and hot soak number 6.

Following cycling the unit was returned to +40C and TQCM data was collected for several hours – see below.

# 4. Temperature Profile



#### STE-U FM2 Thermal Vac, Cycles 4-7



# 5. Trending Data

STE-U PM2 Performance Tren		1										Test Dulasr						Dec	Deor Source				Loss Interation Door Southe (Door LUT)						
							Door	Door				rest numer			10000		Cree	Credit about of					Long meg	any megration Do		Deor Cu I			
Date	File	Test	STE-U Temp	Premep Temp	IDPU Temp	ISTEUCU (mA)	Open (sec)	Close (sec)	Fit Rev	Det.	Thresh.	Offset (keV)	Gain (keWBin)	Curv. (t/keV)	Test. Gain	PWHM (keV)	Offset (keV)	Gain Curv. (keWBin) (1/keV	GiveV cis	22keV c/s	FWHN	AccTime (sec)	Offset (keV)	Gain (keV/Bin)	Curv. (1/keV)	EkeV c/s	225xeV c/s	88keV cis	FWHM
										0	10	-0.00	0.3657	1.09E-04	13,4135	1.034	-0.05	0.3810 Ge-5 (F)	44.97	26.34	1.081		-0.03	0.3807	6.14E-05	42.90	24.09	1.05E-02	1.067
July 21 2004	0407211325.fm	Pre Tiernal vac	23.9	26.3	33.3	35.8	0.3870.38	0.25/0.38	7/14/2004		9	-0.02	0.3848	1.296-04	12,7075	0.884	-0.04	0.3269 66-5 (F)	48.73	26.08	0.932		-0.04	0.3769	69-5 (F)	45.48	23.60	9.31E-08	0.925
		arcent (in chamber)									10	-0.04	0.3653	1.210-04	12.9227	0.933	-0.05	0.3765 58-5 (7)	37.00	24.92	0.914		-0.05	0.3759	58-5 (F)	36.57	21.65	1576-02	0.945
											0	0.04	0.3650	1,116-04	13,9300	0.005	-9.12	0.3625 00-5 (6)	49.00	24.00	6.001	1990	-0.10	0.3650	6 90E //5	30.01	95.18	1,000-00	0.000
		Thermal Vac Hot Soak	-21.8		35.7				100225	1		0.01	0.3545	1.315-04	12 (0501	0.753	-0.01	0.3255 6e-5 (F)	51.63	27.05	0.000		0.00	0.3785	T 27E-05	46.70	24.36	1.745.00	0.545
July 26 2004	0407260000 tm			38,6		10.2	0.38/0.38	0.38/0.38	7/14/2004	2	8	0.01	0 3649	1 205-04	12 8280	0 779	-0.01	0.3783 (e-5 (F)	40.51	23.90	0.997	540	-0.02	0.3784	6e-5 (E)	38.07	22.50	11/16-02	0.879
										3	g	-0.04	0.3652	1.158-04	13 37 10	0 arr	-0.04	0.3629 5e-5 (P)	38.64	24.98	0.963		-0.03	0.3827	5 BEE-05	37.06	22.04	2 812-00	0.978
										0	1	-0.06	0.3657	1.11E-04	13,2480	0.713	-0.02	0.3658 Ge-5 (F)	47.89	26.38	0.821		-0.01	0.3653	6 06E-05	44.75	24.38	2 09E-02	0.856
		Thermal Vac Cold			-	10.00			-	1	6	0.01	0.3851	1.33E-04	12,5321	0.570	0.00	0.3818 6e-5 (F)	50.18	25.00	0.687	1000	0.00	0.3818	0.45E-05	47.02	23.65	2.18E-02	0.683
109 20 2004	0407200000 8m	n Soak #2	-94-0	-404.1	30.4	10.00	0.507 0.30	0.5070.30	711412004		6.	0.01	0.3654	1.31E-04	12.6495	0.615	0.01	0.3011 0.200	05 39.92	23.38	0.000	1000	-0.01	0.3822	5.138-05	37.75	22.35	8-19E-03	D.706
	-	201104000		1000						3	1	-0.05	0.3851	1.16E-04	13,2630	0.683	0.04	0.3655 7.47E-	40.63	25.41	0.795		-0.04	0.3657	5.61E-05	37.29	23.27	1.28E-02	0.785
										0	8.	-0.06	0.3855	1.07E-04	13.3558	0.891	-0.01	0.3822 Be-5 (F)	47.89	26.41	0.903		-0.01	0.3821	6.50E-05	44.52	24.63	1.68E-02	0.912
July 27 2004	0402270000 Bm	Thermal Vac Hot Sook	-22.3	30.5	33 t	48.7	0.38/0.3	0.38/0.38	714/2014	1	7	0.01	0.3647	1.31E-04	12.0527	0.745	0.00	0.3784 6e-5 (P)	51.39	26.04	0.780	2200	-0.01	0.3784	T DØE-05	47.25	23.96	1.508-02	0.792
100 21 2001		#3			- C				C.C. Barrer	2	7	-0.01	0.3848	1.25E-04	12,8316	0.768	-0.02	0.3782 Ge-5 (F)	41.38	24.07	0.809	TANK	-0.01	0.3780	0e-5 (F)	37.93	22.27	1.02E-02	0.811
	-	100		_		-	_			3	4	-0.06	0.3851	1.13E-04	13:3710	0.862	-0.03	0.3824 Be-5 (F)	39.95	23.84	0.872		-0.04	0.3827	5.55E-05	37.16	23.10	1.43E-02	D.889
				-37	34	18.5				0	7	-0.05	0.3851	1.12E-04	13.2577	0.715	-0.01	0.3854 (e-5 (F)	47.49	25.30	0.787		-0.02	0.3657	5.54E-05	45.71	24.82	1.4%E-02	0.811
July 27 2004	0407270000.tm	Thermal Vac Cold	-04.8				0.50/0.5	0 0 50 / 0 5	7/14/2004	1	0	0.00	0.3649	1.29E-04	12.5329	0.578	0.00	0.3820 6e-5 (F)	50.87	25.74	0.688	320	0.01	0.3813	8.62E-05	48.49	23.97	1.19E-02	0.673
100000000000000000000000000000000000000	0407270937.8m	Boak #3 (cold start)							00000000	3	0	0.01	0.3850	1.30E-04	12.6485	0.603	-0.01	0.3523 Ge-5 (P)	41.62	24.50	0.6565		-0.01	0.3893	5.24E-05	37.99	22.79	1.388-00	0.704
		<u> </u>									1	-0.05	0.3657	1.14E-04	13,2980	0.676	-0.04	0.3857 0e-5 (F)	40.80	24.98	0.785		-0.04	0.3863	7.64E-05	37.38	23.07	1.82E-02	0.780
	0407270937 fm	Thernel Vac Hot Soak			32.7	95.4			Same	0	8	-0.04	0.3855	1.11E-04	13,3596	0.839	0.00	0.3821 66-5 (F)	47.49	26.53	0.907		-0.02	0.3825	69-5 (F)	44.32	24.33	1.42E-03	0.913
July 27 2004			-22.7	38.6			0.38/0.3	0.38/0.38	7/14/2004		7	0.01	0.3850	1.31E-04	12.0501	0.702	-0.02	0.3767 Se-5 (P)	50.54	25.67	0.794	530	0.00	0.3764	6e-5 (F)	47.00	Z3 91	1 202-02	0.794
		84							1992	2		0.01	0.3648	1.27E-04	12.8241	0.720	0.01	0.3776.08-5.0F)	41.57	25.18	0.812		-0.01	0.3780	00-0 (F)	31.12	22.58	8.75E-08	0.810
											4	-0.00	0.3852	1.150-04	13.3962	NUS D	-0.02	0.3822 68-5 (P)	39.48	25.10	0.889		-0.04	0.3821	1.6VE-05	38.92	23.25	2.12E-02	0.555
		Thermal Vac Cold		-30	32.4		0.507.0.50					-0.04	0.3652	1.12E-04	13,2099	0.814	-0.02	0.3863.08-5.0-1	48.50	20.99	0.947		-0.02	0.3868	0.14E-00	40.58	29.20	1.005-02	0.933
Aug 5 2004	0408051114.8m		-97.7			18.5		0.38/0.50	6/5/2004			-0.01	0.3546	1.27E-04	12,7853	0.715	-0.01	0.3521 68-5 (F)	49.77	25.45	0.184	800	-0.02	0.3616	179E-09	46.20	23.43	1.24E-02	0.098
		OLAR, #4										-0.01	0.3000	1.230-04	13.0427	0.069	-0.01	0.3620 56-5 (7)	40.13	23.43	1 040		-0.01	0.3017	5 510-05	31.44	22.19	1.300-00	0.021
											10	0.00	0.3642	1 195 04	10.2710	1.021	0.04	0.3655 85 5 (5)	44.00	45.00	1.021		0.00	0.3670	0.275.00	60.00	21.04	1,005,02	1.007
	0408051114 800	Thermal Vice Hot Sould	4 -20.7	39.6							10	0.00	0.0004	1.120-04	12,0122	0.007	-0.01	0.3035 68-5 (F)	40.57	35.30	0.977		-0.03	0.0001	0.00C-00	40.01	24.00	D.00E+02	0.041
Aug 5 2004	0408052157 8m	85			33.8	10.3	0.38/0.38	0.25/0.38	8 8/5/2004			-0.01	0.3646	1 215-04	13 2138	0.901	-0.02	0.3774 Ge-5 (E)	39.74	24.91	0.904	360	-0.03	0.3775	6e-5 (E)	37.04	22.13	1125-02	0.958
											10	.0.05	0 1857	1.145-04	13,4175	1.019	-0.09	0.5844 Be-5 (E)	38.68	24.70	1.095		4.05	0.3841	BASIE)	99.97	23.17	8.74E-03	1.082
										0	11	-0.05	0.3654	1 136-04	13 2905	6.911	-0.02	0.3868.0e-5 (E)	48.33	26.04	6.959		-0.01	0.3663	0.546-05	65.00	26.34	2 736-02	0.885
	0408052157 fm	Thermal Vac Cold Soak #5	-90	-31.4	32.1	18.5	0.5070.50		405030	1		0.00	0.3646	1 265-04	12 7779	0.743	.0.01	0.3622 Bo 5 (E)	50.47	25.42	0.825		0.00	0.3813	A 95E-04	49.18	23.61	1455.10	0.750
Aug 5 2004	0408060000 tm							0.38/0.50	85/2004		10	-0.01	0.3840	1,23E-04	13.0482	0.764	-0.01	0.3615 Ge-5 (F)	40.54	24.09	0.250	040	-0.03	0.3810	5 DEE-05	37.15	22.15	1.11E-00	0.774
										3	11	-0.06	0.3857	1.13E-04	13,2957	0.882	-0.05	0.3676 Ge-5 (F)	39.35	24.13	0.949		-0.05	0.3672	6.30E-05	36.74	22.67	1.13E-02	0.875
		Sectors and the sectors and								0	10	-0.05	0.3656	1.12E-04	13.4080	1.034	-0.03	0.3830/6e-5 (F)	47.91	26.75	1.070		-0.03	0.3853	69-5 (F)	44.94	24.40	3.55E-08	1.079
A	0.400000000 Rev	Thermal Vac Hot Soak	-20.7	45	31.7	18.3	0.00.000	0.00 10.00		1	8	0.00	0.3840	1.27E-04	12.9280	0.872	-0.02	0.3784 6e-5 (7)	50.04	25.48	0.942	200	-0.01	0.3781	6e-5 (F)	47.19	24.14	3.302-03	0.941
A00 0 2004 0	0408000000 Bh	#B					0.3870.38	0.38 ( 0.38	85/2004	09	9	0.00	0.3850	1.21E-04	13,2105	0.901	-0.02	0.3777 Ge-5 (F)	41.62	24.20	0.977	350	-0.02	0.3779	6e-5 (F)	37.00	22.82	121E-02	0.953
										3	10	-0.06	0.3858	1.13E-04	13.4147	1.021	-0.04	0.3842 6e-5 (F)	37.40	24.63	1.040		-0.08	0.3847	66-5 (F)	36.40	23.25	1.06E-02	1.077
		Contraction and the second		-32.3	32.3					0	9	-0.07	0.3854	1.10E-04	13.2513	0.891	-0.04	0.3874 6e-5 (F)	47.78	26.00	0.957		-0.02	0.3868	5.83E-05	44.64	24.19	2.80E-02	0.909
Aug 5 2004	0.0000000000000000000000000000000000000	Thermal Vac Cold	-95.4			100.00	0.0010.00	0.75 (0.00	-	1	8	-0.01	0.3850	1.26E-04	12,7677	0.728	-0.02	0.3823 6e-5 (F)	48.41	25.48	0.813	100	-0.02	0.3621	5.70E-08	48.43	23.28	9.95E-08	0.817
	0408060000 811	Soak #8				10.3	0.507 0.5	0.3610.50	0.35004	2	4	-0.02	0.3851	1.216-04	13.0313	0.757	-0.04	0.3825 6e-5 (7)	41.05	24.24	0.850	D.JU	-0.01	0.3617	6e-5 (F)	36.55	22.26	1.428-02	0.842
		230-24								3	9	-0.00	0.3850	1.13E-04	13.2024	0.880	-0.05	0.3876 Ge-5 (F)	38.41	25.30	0.963		-0.05	0.3673	5.96E-05	36.66	22.52	1.07E-02	0.946
		Thermal Vac Hot Soak 97	-27.5	39.1	34	10.2				0	9	-0.04	0.3653	1.13E-04	13.3631	0.983	-0.02	0.3835 6e-5 (F)	45.48	24.54	1.043		-0.02	0.3837	5.26E-05	44.79	24.49	1.56E-02	1.043
Aut 6 2004	0408060000 Bm						0.38/0.38	0.38/0.38	85/2004	1	4	-0.01	0.3846	1.258-04	12.8540	0.025	0.00	0.378D Se-5 (P)	49.68	25.45	0.916	810	-0.01	0.3783	6e-5 (F)	46.65	23.67	6 DOE-00	0.899
. and a state	0408061733.8m						N.361 Q.38		- and -	2		-0.01	0.3854	1.20E-04	13,1941	0.854	-0.01	0.3778 Ge-5 (F)	39.67	24.67	0.915		-0.02	0.3778	6e-5 (F)	37.09	22.41	194E-02	0.927
	-									3	9	-0.05	0.3652	1.15E-04	13.3898	0.975	-0.05	0.3844 6e-5 (F)	36.89	24.28	1.044		-0.05	0.3846	5.04E-05	36.30	22.91	1.53E-02	1.039
										0		-0.04	0.3850	1.14E-04	13,2631	0.892	-0.02	0.3866 6e-5 (F)	48.27	25.64	0.943		-0.03	0.3669	5.02E-05	45.68	24.72	9.55E-08	0.985
Aug 5 2004	0408001733.8m	Thermal Vas Cold	-80.1	-29.2	34.5	96.3	0.50/0.50	0.38/0.50	0/5/2004	-1	1	0.00	0.3846	1.29E-04	12,7789	0.732	0.02	0.3820 6e-5 (F)	50.52	25.89	0.823	810	-0.02	0.3817	89-5 (F)	48.29	23.82	1 34E-02	0.819
		500K #7								2	4	-0.10	0 3850	1.22E-04	13.0497	0 761	-0.02	0.3817 6e-5 (P)	41.19	23.64	0.817		-0.02	0.3615	Ge-5 (F)	37.47	22.58	5 33E-03	0.847
						_				3	9	-0.07	0.3857	1_14E-04	13,2977	0.879	-0.05	0.3875 6e-5 (F)	39.53	24.31	0.940		-0.04	0.3867	T.85E-05	36.40	23.15	14/E-02	0.964

#### 5.1. Trending Data Explanation

The trending data on the previous page is extracted from the trending file for this instrument. It is composed of vales measured during the CPT, either directly, or from a post-processing fitting function which evaluates the data collected.

- The Door Open and Door Close columns show two times; from application of power to the time when the door comes off the first switch (starts moving), and the time from the application of power to the time when the door reaches the destination switch.
- Threshold values are DAC levels, corresponding to ~140eV per step. Requirement is <5keV.
- The test pulser fit data measures the electronic performance. Of particular interest is the FWHM, which measures the electronic noise in the system. Other values can be used to look for thermal drift and other trends in energy gain and offset.
- The "door source" fit data measures the calibration source on the STE door, and so is a end-to-end measurement (albeit using mostly photons rather than electrons). Again the FWHM is of interest (requirement < 2keV).

# 6. TQCM Data

A final TQCM value of approximately 47 Hz/hour was reached monitoring a -20C TQCM at 5.0 minute intervals for 30 hours with the chamber shrouds, baseplate, and coldplate set to 40C (non-op hot). This TQCM value indicates only the background levels of contamination from the chamber are present, as was expected from such a small instrument in a large chamber. The TQCM data follows.

Note also the correlation of TQCM rate with room temperature. This run was done during a relatively hot spell; data taken earlier, at the end of the first run, when the room temperature was a bit cooler, achieved rates of ~30Hz/hour.

# 6.1. STE-U FM2 TQCM Data

